

# Comparison of CFD models for multiphase flow evolution in bridge scour processes

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# Introduction

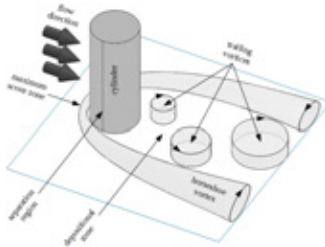
- Erosion is one of the most potentially hazardous environmental phenomena in semi-arid regions (UNEP, 2000).
- Scour has been the cause of more than 60% of bridge collapses occurred since the 1950s (Landers, 1992).



Credit of the pictures: Left, S.D. Craig (USGS); Right, P. Johnson (Penn State Univ.)

# Introduction

- The horseshoe vortex is the flow structure that contributes most to the occurrence of scour on bridge piers (Baker, 1979).



- Scour prevention methods (Melville & Coleman, 2000):
  - Flow alterations
  - Armoring protections

# Introduction

- A good comprehension of the flow behavior when passing around cylinders is crucial to protect bridges successfully.
- An extensive literature has addressed this classical problem of fluid mechanics both numerically and experimentally.
- In CFD cases of application, LES is the most used approach.
- LES models are more accurate than RANS, although their computation times are 10 times longer (Rodi, 1997).

## Goal

The aim of this work is to compare two of the most used numerical models in hydraulic engineering applications, namely:

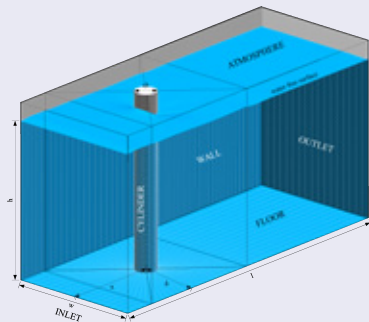
- The open source platform **OpenFOAM**
- The commercial software **FLOW-3D**

## Materials and methods

A case study is run to compare the performance of both models.

### Geometry

- The study case consists of a single cylindrical bridge pier.
- The pier is attached to the bottom of a sandy streambed channel of rectangular walls.
- The results are compared to experimental data obtained in an open sediment transport channel.



# Materials and methods

## Mesh

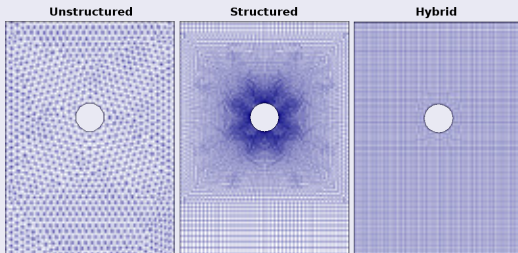
- Three meshing approaches are assessed using OpenFOAM:

Mesh type	Pros	Contras
Unstructured	<ul style="list-style-type: none"> <li>- Refinable</li> <li>- Adaptive</li> </ul>	<ul style="list-style-type: none"> <li>- Problems to reproduce water free surfaces</li> </ul>
Structured	<ul style="list-style-type: none"> <li>- Refinable</li> <li>- Fast simulations</li> </ul>	<ul style="list-style-type: none"> <li>- Poor capability to adapt to complex geometries</li> </ul>
Hybrid	<ul style="list-style-type: none"> <li>- Adaptive</li> <li>- Fast simulations</li> </ul>	<ul style="list-style-type: none"> <li>- Bad refinement in solid contour vicinity</li> </ul>

# Materials and methods

## Mesh

- The third option (hybrid meshing approach) is considered the most suitable in the OpenFOAM case.
- The same approach using the FAVOR method is the only option in FLOW-3D.





# Materials and methods

## Numerical model

- The Saint-Venant and the Boussinesq Equations can model the flow around cylinders with some simplifications.
- A full three-dimensional approximation of this kind of flow can only be done approximating the Navier-Stokes Equations.
- The Navier-Stokes Equations are discretized using the Finite Volume Method (FVM), see Versteeg & Malalasekera (2007).
- The treatment of two coexisting flows is done using the Volume of Fluid (VOF) approach (Hirt & Nichols, 1981).
- The VOF implementation and how water-air interfaces are tracked differs slightly from one model to the other.

# Materials and methods

## Numerical model

- The flow turbulent fluctuations are fully modeled using the RNG RANS  $k-\varepsilon$  model (Yakhot *et al.*, 1992).
- Simulations are run using a Courant-dependent variable time step algorithm to ensure convergence.
- Simulations are considered to have converged when the domain turbulent kinetic energy and volume of water stabilize.
- Variables are averaged using a 4-second window (one order of magnitude larger than quasi-periodic phenomena periods).
- Variables are obtained only from  $3.75\phi$  upstream of the pier to  $28.00\phi$  downstream of it to minimize the BC effects.

# Materials and methods

## Boundary conditions

- Inlet:** constant water depth and inlet velocity and null  $k$  &  $\varepsilon$  (an initial reach is simulated for the flow to develop).
- Outlet:** constant water depth (hydrostatic profile imposed) and null Neumann condition for the rest of variables.
- Sky:** atmospheric boundary condition (the flow can freely leave the domain with no gradients whatsoever).
- Walls:** no-slip condition and high-Reynolds-number rough wall function to reduce computation times.

# Materials and methods

## Case study

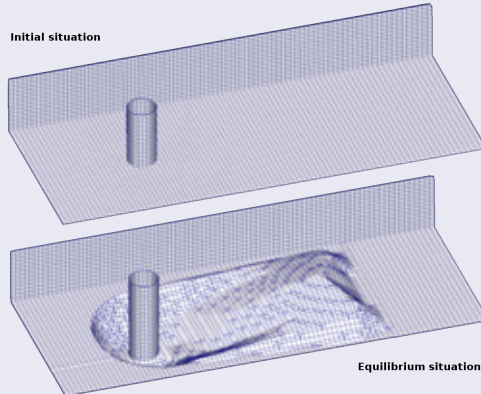
The case study is aimed at comparing both numerical models, OpenFOAM and FLOW-3D, using experimental data:

- Channel dimensions:  $0.800m \times 0.064m$
- Pier diameter:  $\varnothing = 0.0107m$  (at  $L_1 = 0.300m$  from inlet)
- Sand grain diameter:  $d_s \in [0.40, 0.63]mm$
- Flow rate:  $q = 0.75 \cdot 10^{-3} \frac{m^3}{s}$
- Water level:  $h_{inlet} = 0.0792m$ ,  $h_{outlet} = 0.0786m$
- Diameter-based Reynolds number:  $Re = 1,570$
- Approaching Froude number:  $Fr_1 = 0.167$

# Materials and methods

## Case study

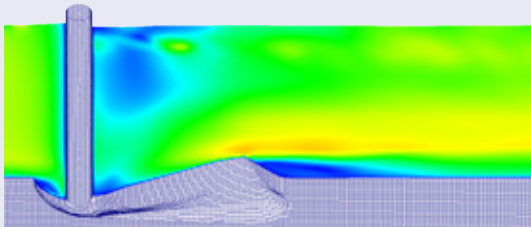
- Two scenarios are considered:



# Materials and methods

## Case study

- A mesh sensitivity analysis for four different element sizes ( $\Delta x = [5, 4, 3, 2]mm$ ) is conducted using the variables:
  - Recirculation zone length ( $L_D$ )
  - Vortex shedding period ( $T_{VS}$ )
  - Max. vertical dimensionless coordinate ( $y_{max}^+$ )



# Analysis of results

## Reproduction of the physics

- The results reproduce the physics of the problem observed at the experimental facility in both cases.
- Stagnation produces a water level rise upstream of the pier.
- A water level descent occurs downstream of the pier due to flow acceleration.



## Analysis of results

### Mesh sensitivity analysis

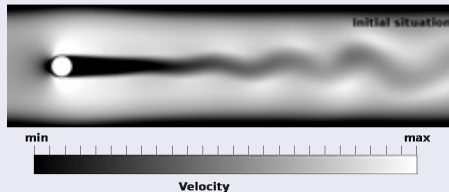
- The three variables analyzed showed no significant improvement beyond a mesh size of  $\Delta x = 3mm$ .
- Computational times soar when using finer meshes.
- The maximum  $y^+$  coordinate of the elements in touch with solid boundaries converged in both models to 60.
- The recirculation length ( $L_D$ ) converged to  $0.406m$  and  $0.418m$  in OpenFOAM and FLOW-3D, respectively.



# Analysis of results

## Mesh sensitivity analysis

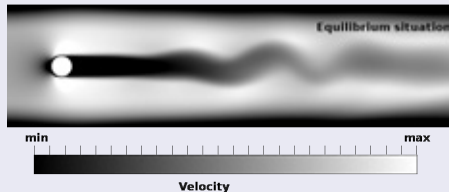
- The vortex shedding period ( $T_{VS}$ ) converged to 0.334s and 0.414s in OpenFOAM and FLOW-3D, respectively.
- Blevins' (1990) method to estimate the Strouhal number as a function of the diameter-based Reynolds number is used.
- $T'_{VS} = 0.372s$  is obtained, which implies a relative error of -10.2% and 11.3% in OpenFOAM and FLOW-3D, respectively.



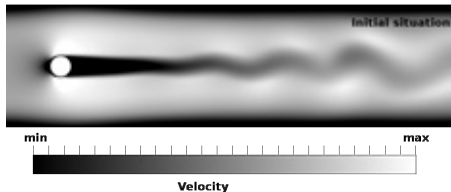
# Analysis of results

## Mesh sensitivity analysis

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## Analysis of results

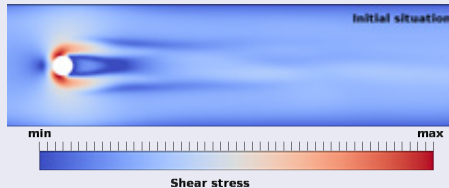


Play video

## Analysis of results

### Shear stress

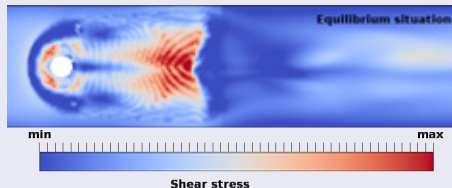
- The largest shear stress in the initial situation occurs where the horseshoe vortex forms (future scour hole location).
- The smallest value corresponds to the region where the sediment mound will eventually appear.



# Analysis of results

## Shear stress

- In the equilibrium situation, the shear stress becomes lower and more uniform in the pier vicinity.
- Unexpectedly large stresses occur on the sediment pound that can overcome the critical shear stress ( $\tau_c$ ).
- The Shield's diagram cannot foresee the triggering of erosion processes on uneven streambeds. Is  $\tau_c$  useful? Does it exist?



# Conclusions

- A comparison of performance of OpenFOAM and FLOW-3D applied to hydraulic structure modeling is presented.
- A study case is conducted using both codes and experimental data obtained in an open sediment transport channel.
- Both models manage to reproduce the physics of the problem under study and all variables converged to stable solutions.
- OpenFOAM slightly overestimates the recirculation length in detached flows with respect to FLOW-3D results.
- Compared to Blevins' (1990), OpenFOAM underestimates the vortex shedding period, whilst FLOW-3D overestimates it.
- Large shear stresses are estimated in zones where scour will occur, while lower values are found in deposition regions.
- It is observed that the presence of a scour hole weakens the wake vortex formation to a certain extent.

**Thank you very much for your attention!**

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